

# Reliability of New SiC BJT Power Modules for Fully Electric Vehicles

Alexander Otto<sup>1</sup>, Eberhard Kaulfersch<sup>2</sup>, Klas Brinkfeldt<sup>3</sup>, Klaus Neumaier<sup>4</sup>, Olaf Zschieschang<sup>4</sup>, Dag Andersson<sup>3</sup>, Sven Rzepka<sup>1</sup>

[alexander.otto@enas.fraunhofer.de](mailto:alexander.otto@enas.fraunhofer.de)

Micro Materials Center, Fraunhofer ENAS  
Technologie-Campus 3, 09126 Chemnitz, Germany

<sup>1</sup>Fraunhofer ENAS

<sup>2</sup>Nanotest und Design GmbH

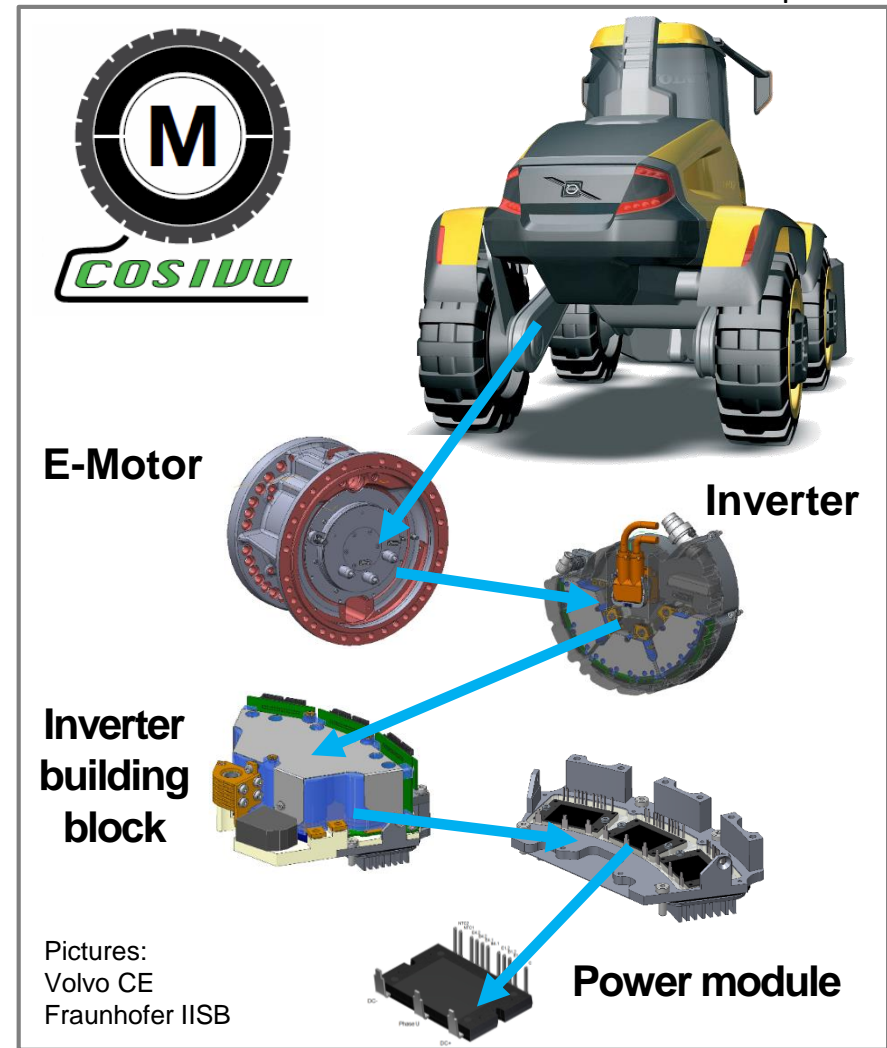
<sup>3</sup>Swerea IVF AB

<sup>4</sup>Fairchild Semiconductor GmbH

# I. COSIVU project | Overview

## Project objectives:

- Development of a novel electric drive-train system architecture by realizing a smart, compact, and durable single-wheel drive unit including:
  - integrated electric motor
  - 2-stage gear system
  - inverter with SiC based power electronics
  - novel control and health-monitoring system with wireless communication
  - advanced ultra-compact cooling solution
- Validation platform: commercial vehicle (VOLVO) + passenger car (Elaphe)



## II. SiC power module | General information

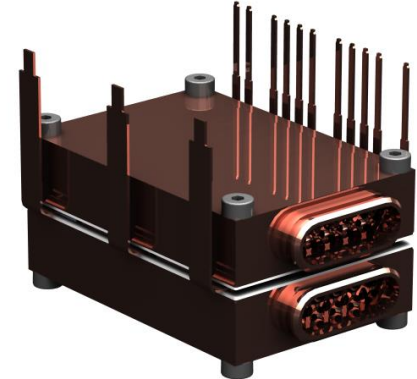
### Power module in half-bridge configuration with full SiC components:

- 4x SiC bipolar junction transistors (BJT) from FCS
- 4x SiC diodes from Cree
- 1200V, 50A (diode: 54A)
- Substrate: DCB with aluminum nitride (AlN) as ceramic isolator
- Lead-free solder; Alu wire-bonds (E: 300 $\mu$ m, B: 150 $\mu$ m)
- Encapsulation: epoxy mold compound (EMC)

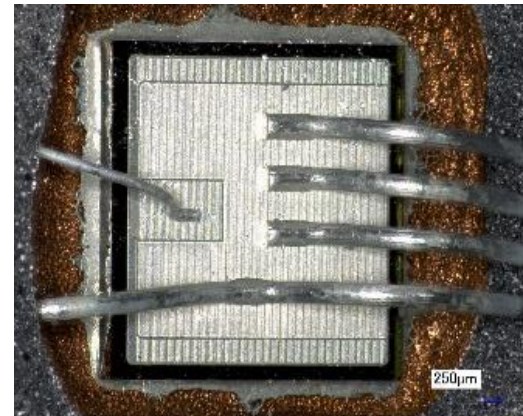
FCS SiC power module:



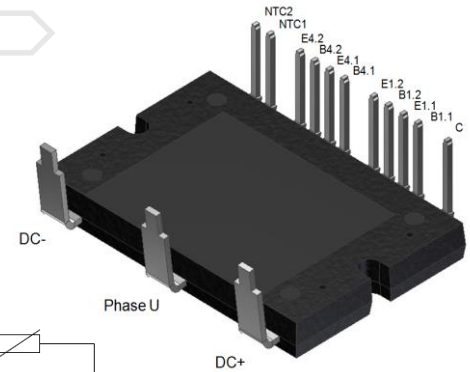
Double-sided cooled SiC power module:



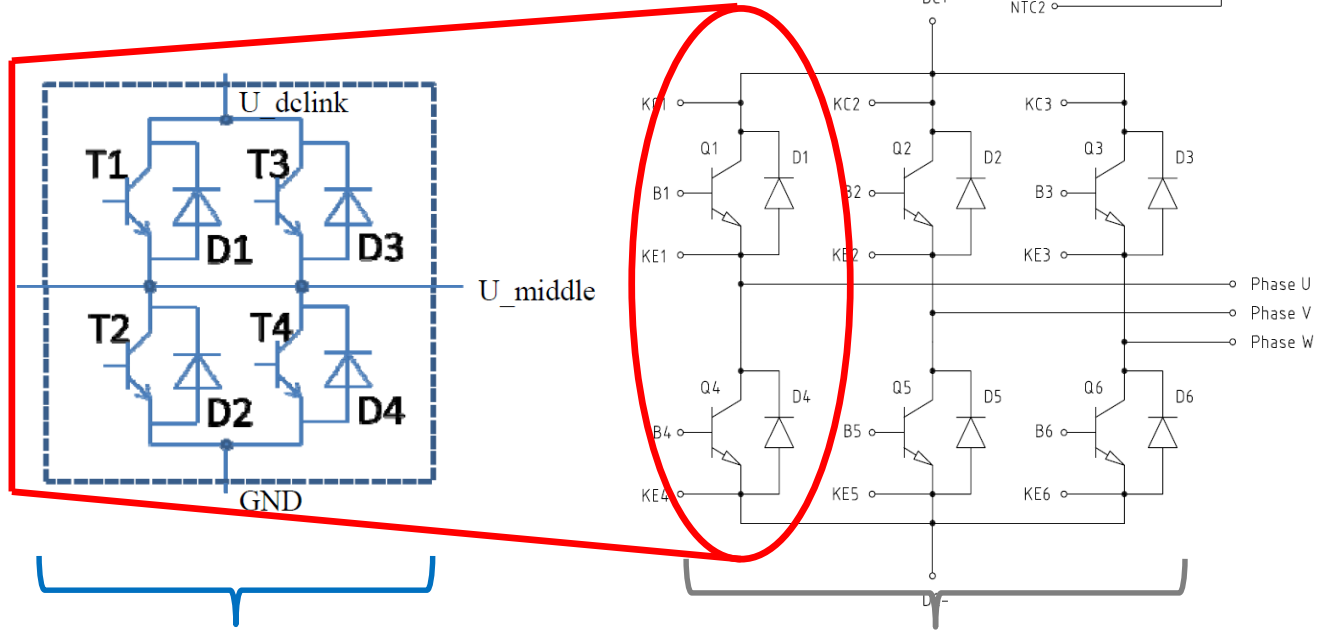
SiC bipolar junction transistor:



# II. SiC power module | Schematic



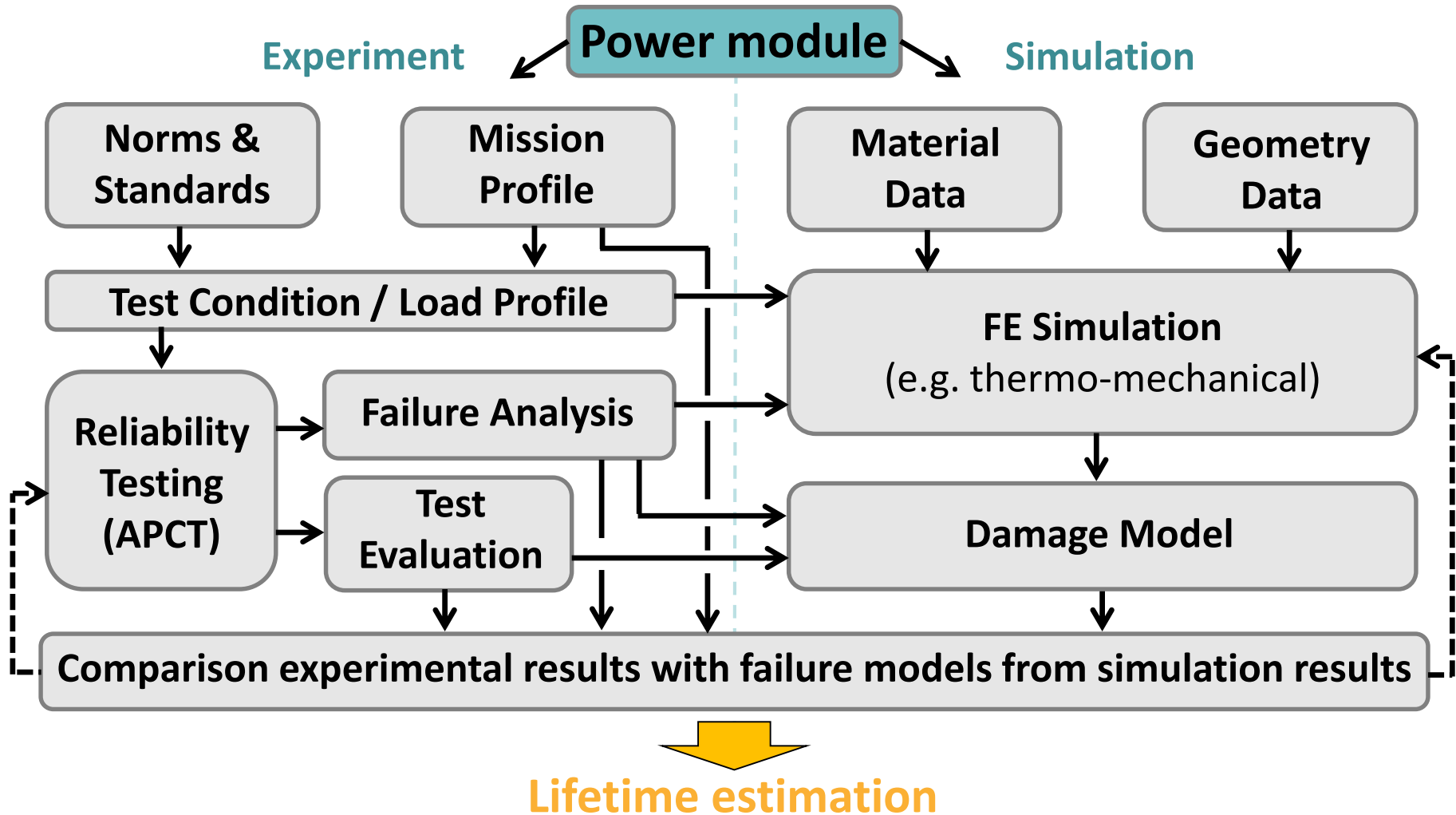
3 power modules in parallel per phase leg



**Power module**  
(half bridge configuration)

**Inverter with 3 phase legs**

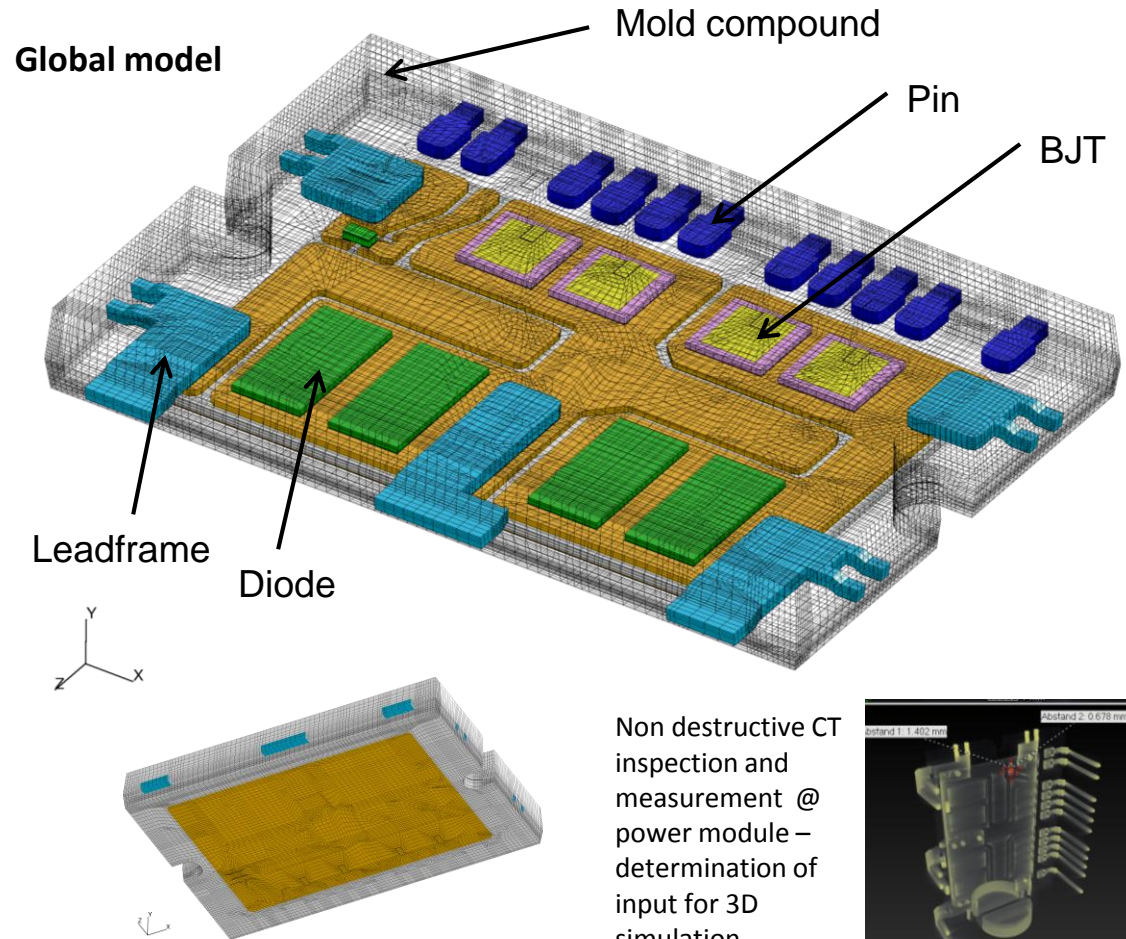
### III. Reliability | General approach for reliability assessment of power module



## III. Reliability | FE simulation: Geometry model

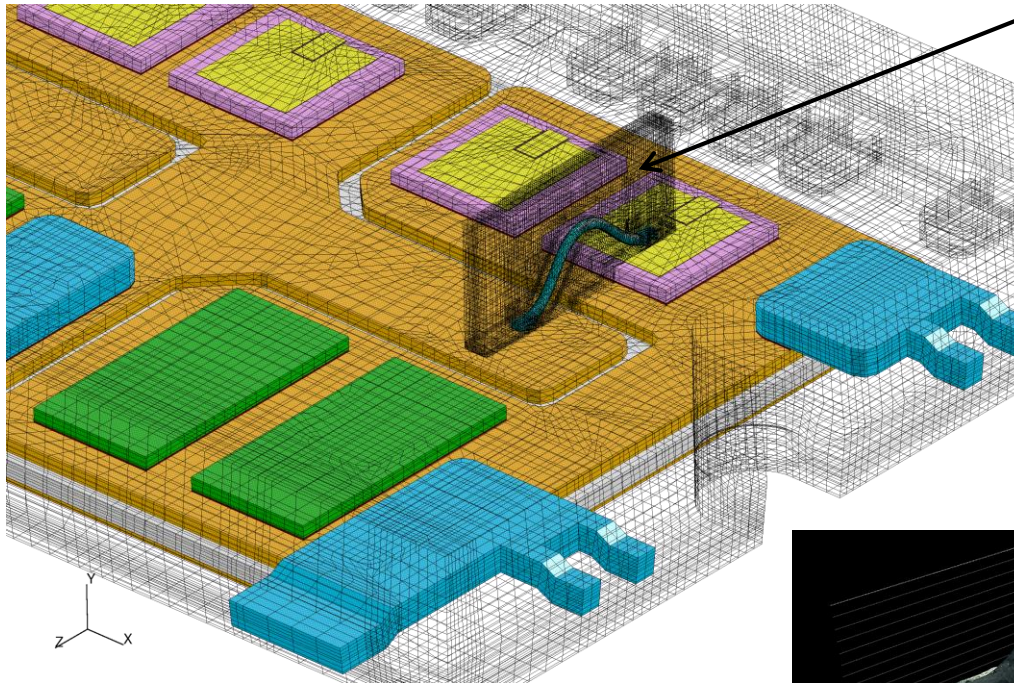
### FE simulation targets:

- Investigation of mechanical stress concentration and accumulating plastic and creep strain induces by:
  - Manufacturing process (soldering of DCB, transfer molding)
  - Internal and external thermal loads
- Replication of the corresponding physical effects

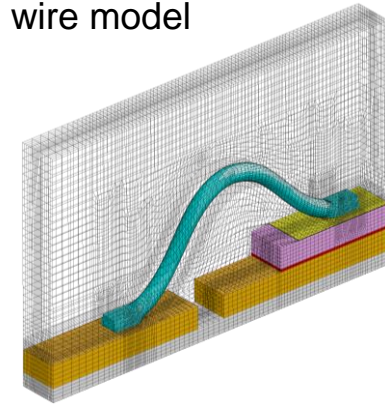


# III. Reliability | FE simulation: Geometry model

## Local geometry model of wire bond:

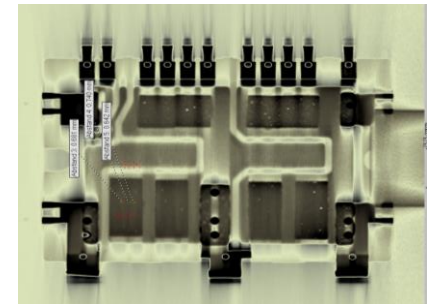
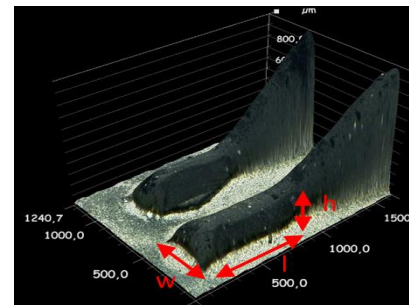


Position of local bond wire model



Position of bond wire derived from CT scan:

3D image of wire-bonds:



## III. Reliability | FE simulation: Geometry model

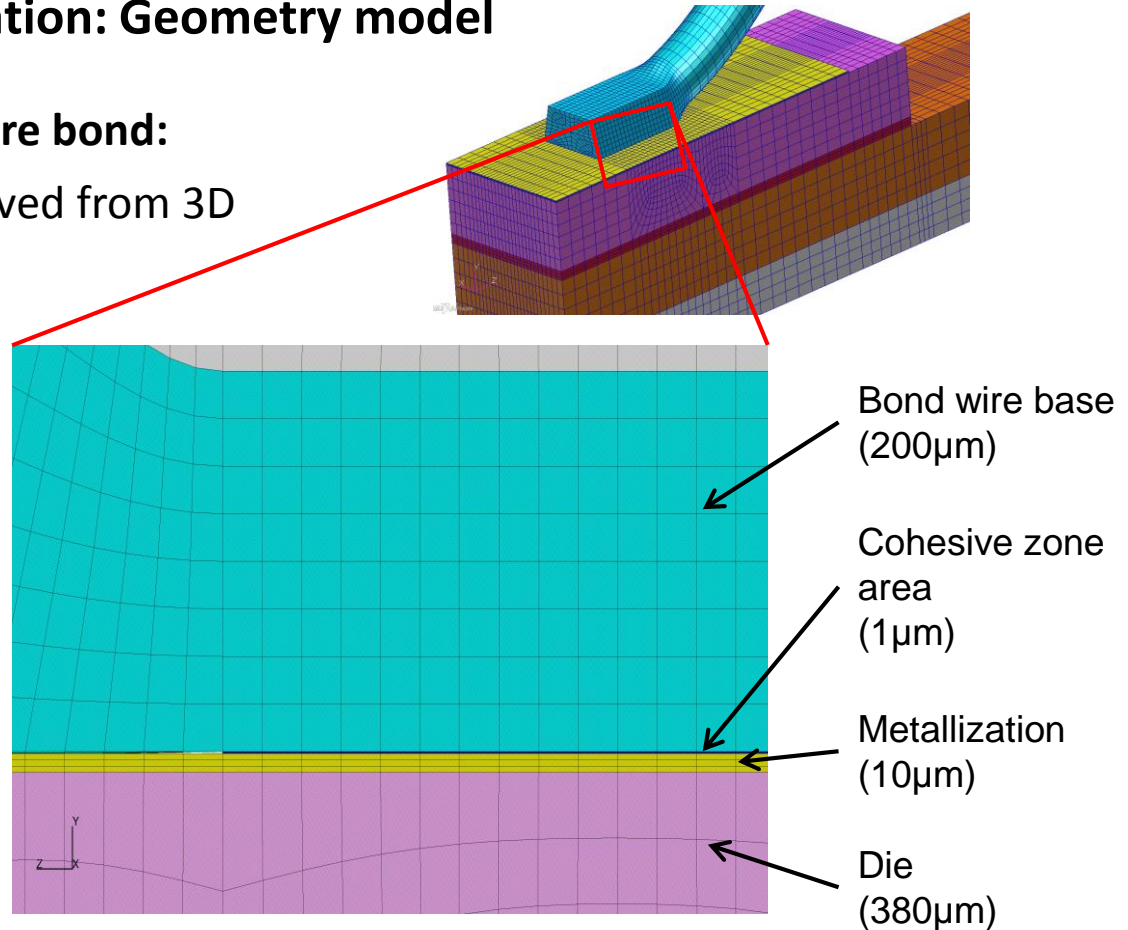
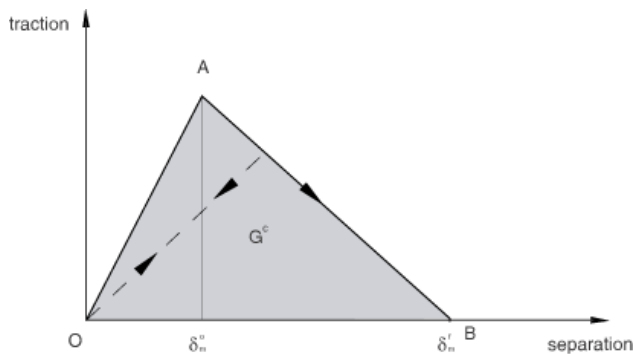
### Cohesive zone approach for wire bond:

- Geometry information derived from 3D digital microscope images

Crack growth law  
(Paris and Erdogan):

$$\frac{da}{dN} = C \Delta K^m$$

Linear traction-separation response:

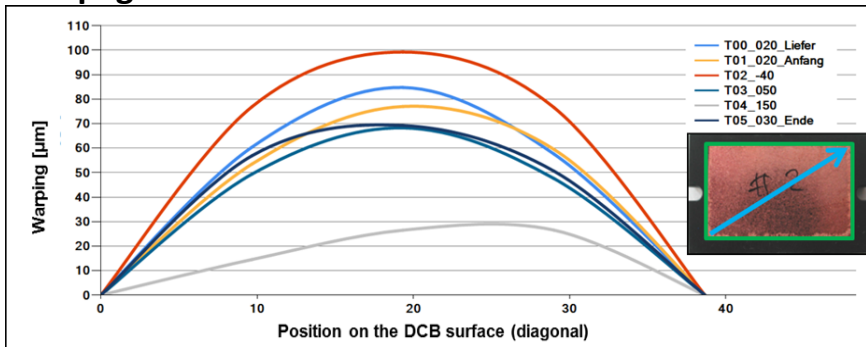




## III. Reliability | FE simulation: Calibration

**Calibration result:** Good compliance between warpage measurement and simulation

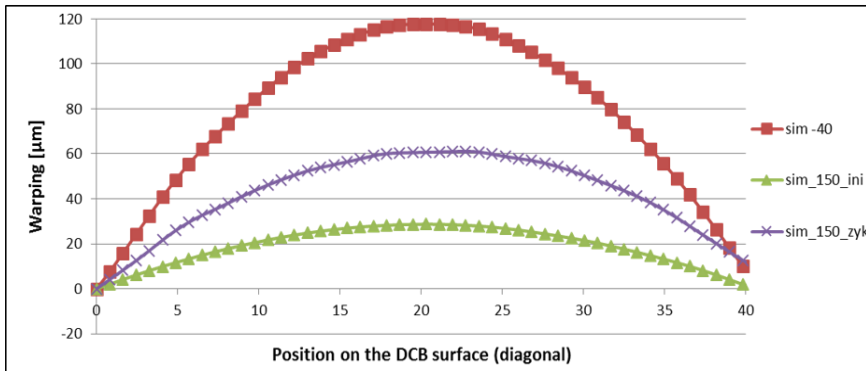
### Warpage measurement results:



### OMI Equinox:



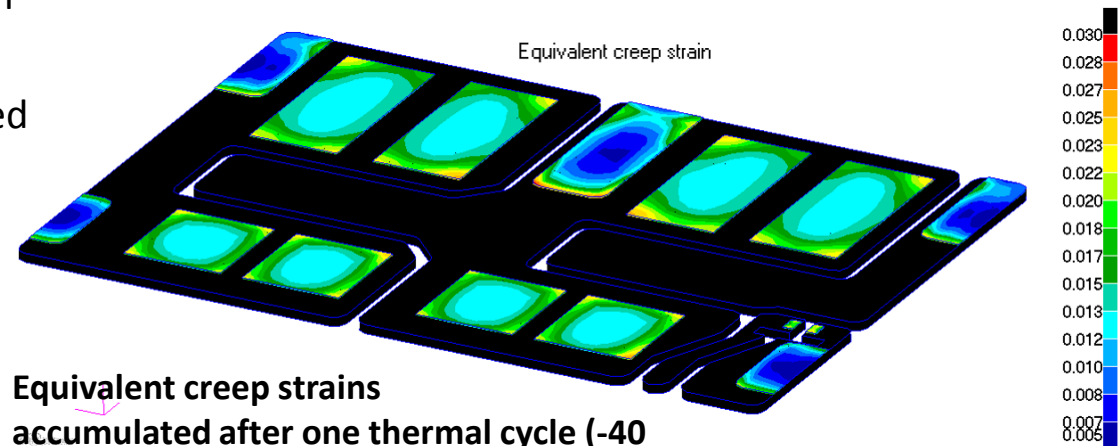
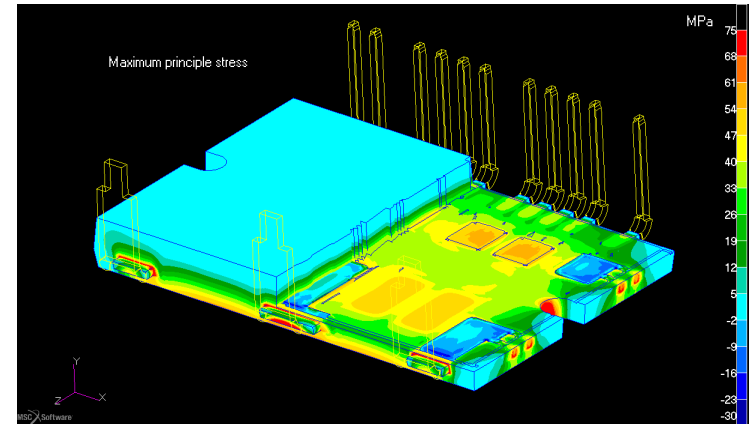
### Simulation results:



## III. Reliability | FE simulation: First simulation results

### FE simulation results:

- Quantifying of creep strains in the die attach of the SiC dies accumulated over the process steps and through thermal cycling already by global model
- Significant strains and stress can be observed in the die attach
- Results indicate that creep strain are primarily influenced by the high CTE mismatch between DCB and SiC dies
- Accumulating equivalent creep strain (=failure criterion) in die attach may lead to solder fatigue

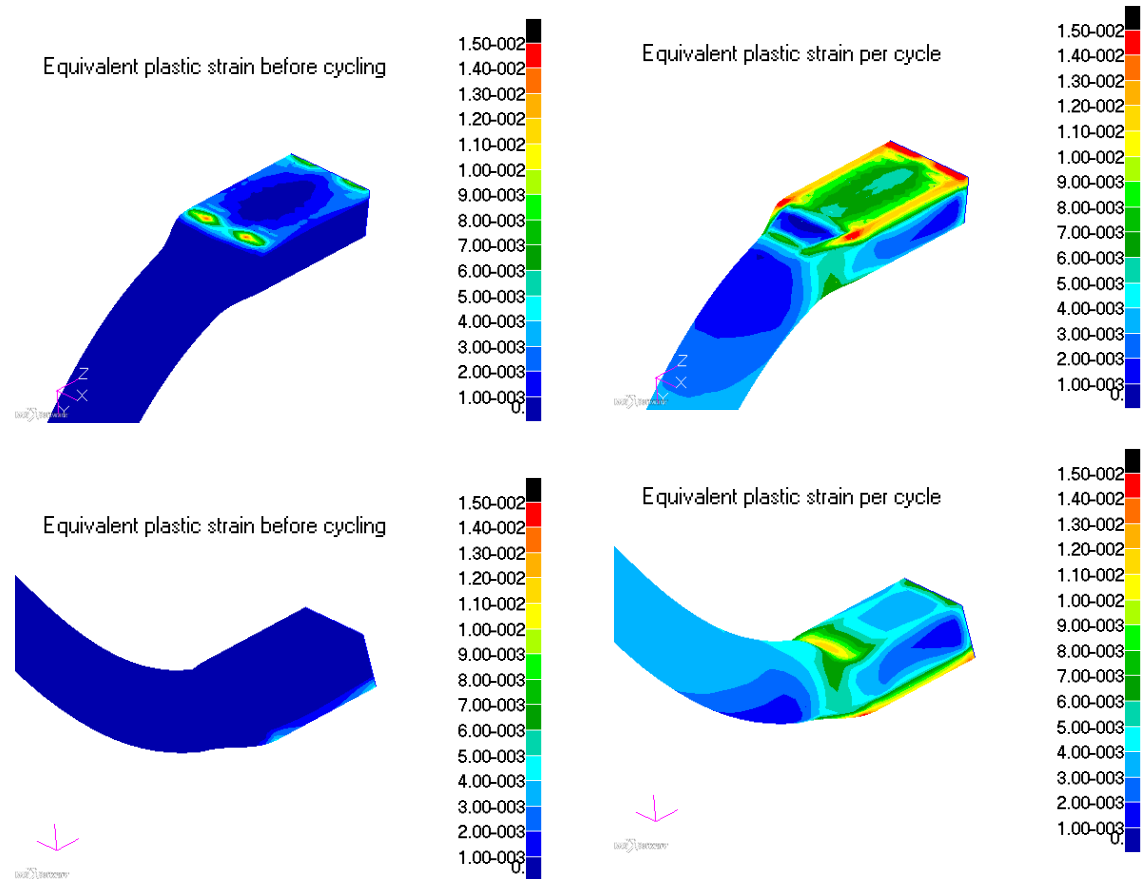


Equivalent creep strains accumulated after one thermal cycle (-40 to 150°C)

## III. Reliability | FE simulation: First simulation results

### FE simulation results:

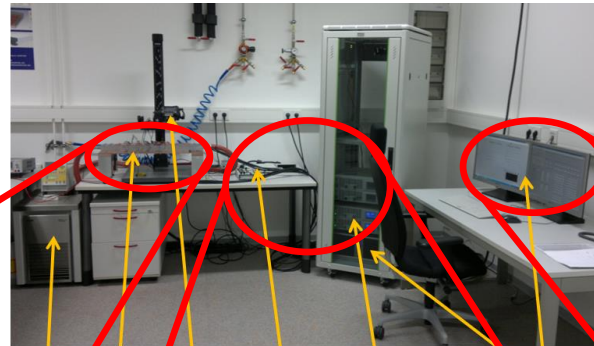
- Monitoring of mechanical stress concentration and plastic deformation at the bond wires have been performed by using the local model
  - Strain values are significant, but conclusions can only be made together with the testing results
- **Further investigations are needed**



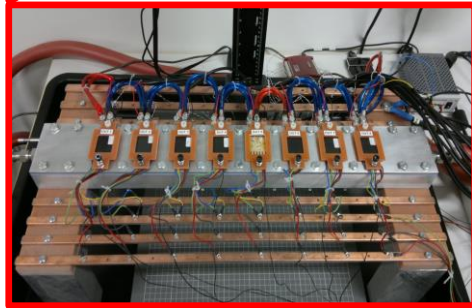
## III. Reliability | Active power cycling: Test bench adaption

**Starting point:** Existing APC test bench dedicated to MOSFET / diode based power modules

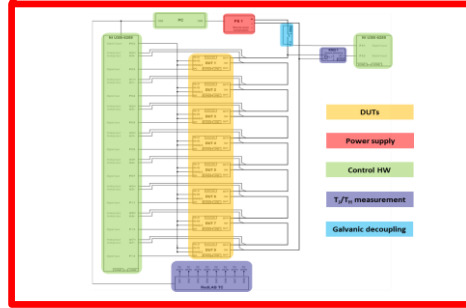
APC test bench at  
Fraunhofer ENAS:



Thermostat    IR-Camera    Power Supplies    PC with control / monitoring SW (LabVIEW)  
Sample holder    Control / monitor HW



1. Sample holder



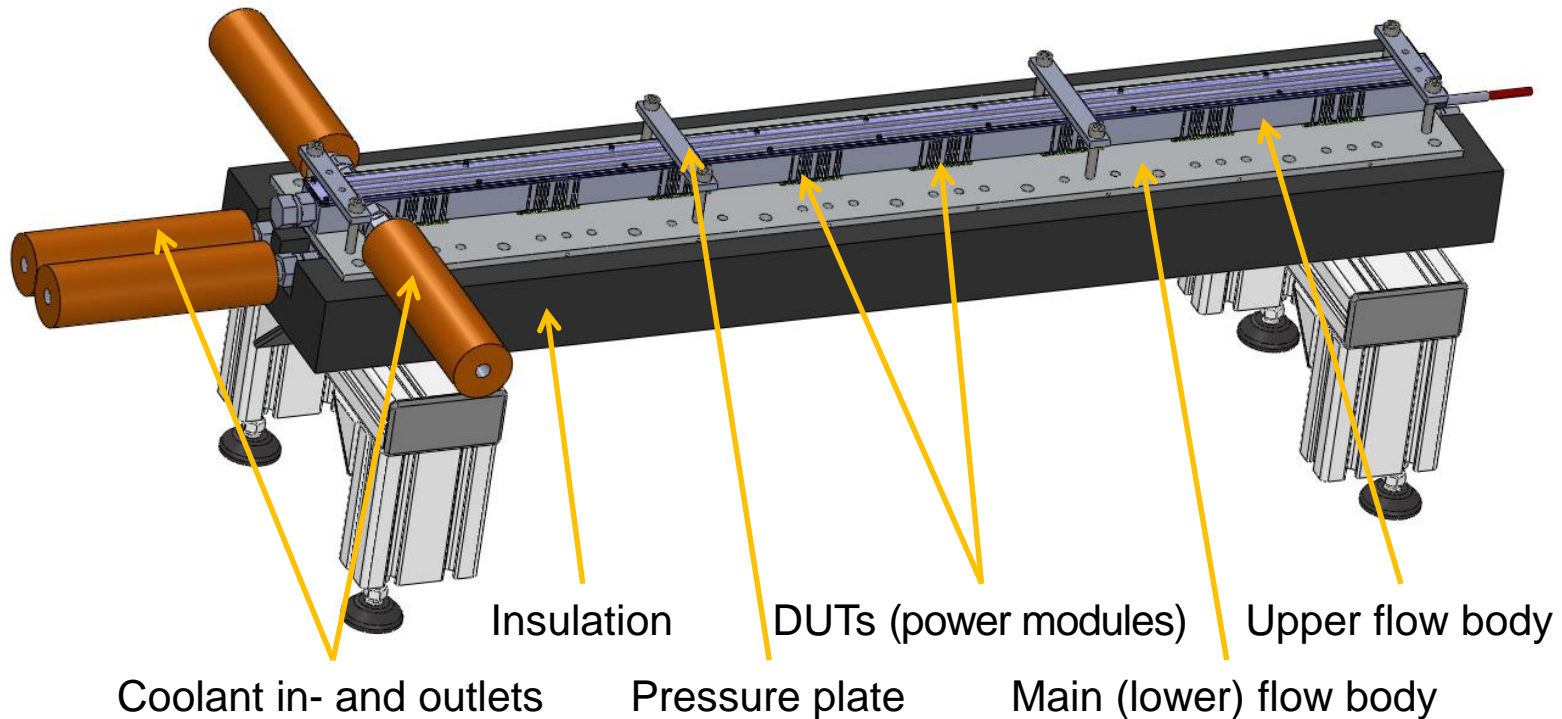
2. Electrical HW / connection plan



3. LabVIEW control SW

## III. Reliability | Active power cycling: New sample holder design

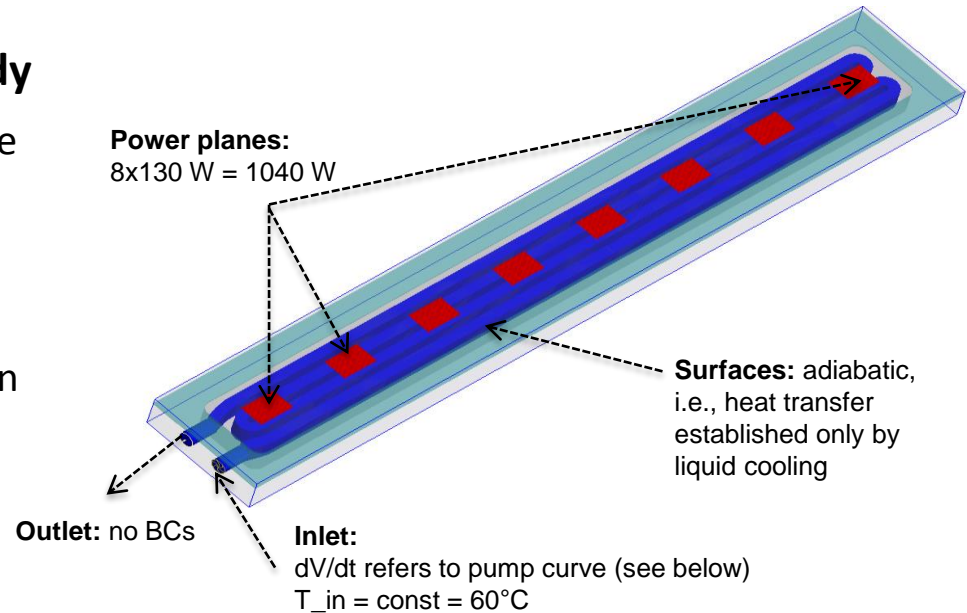
For single-sided + double-sided cooling



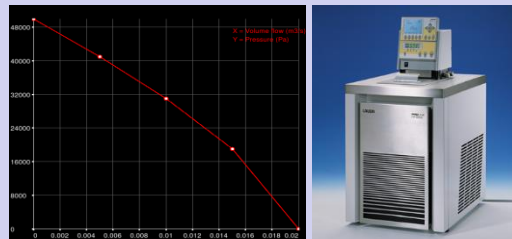
## III. Reliability | Active power cycling: Thermal analysis of cooling body

### Thermal-fluid analysis of cooling body

- Simulation of single-sided cooling case
- Power modules replaced by simple heat sources (130W@50A/1,3V) with constant power
- Employment of steady-state simulation
- Fluid flow rate is determined by the pump system curve



Pump curve of used thermostat (Level 4):



Properties of flow body:

	Chasis material (Alu)	Sealing material (Noarlon 100)
Coeff. of thermal conductivity	313,0 W/mK	0,25 W/mK
Density	19281,0 Kg/m <sup>3</sup>	1700,0 Kg/m <sup>3</sup>
Doeff. of spec. heat	131 KJ/KgK	1300 KJ/KgK

Properties of coolant (Silicon oil Kryo 51):

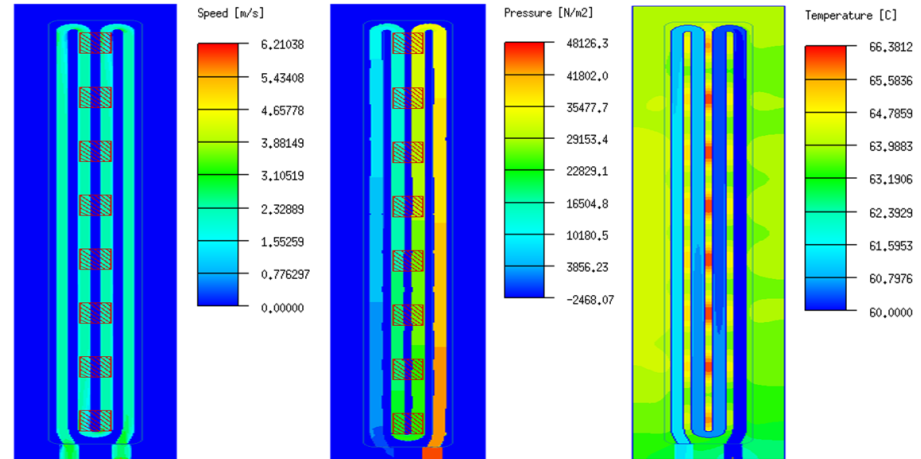
Temaperature degC	kin. viscosity mm <sup>2</sup> /s	dyn. viscosity kg/(m s)	Density kg/m <sup>3</sup>	Spec.
				Heat Capacity KJ/(KgK)
20	5	4.63E-03	925	1.61
40	4.1	3.79E-03	905	1.65
60	3.4	3.15E-03	895	1.68
80	2.6	2.41E-03	875	1.71
100	2	1.85E-03	865	1.73

## III. Reliability | Active power cycling: Thermal analysis of cooling body

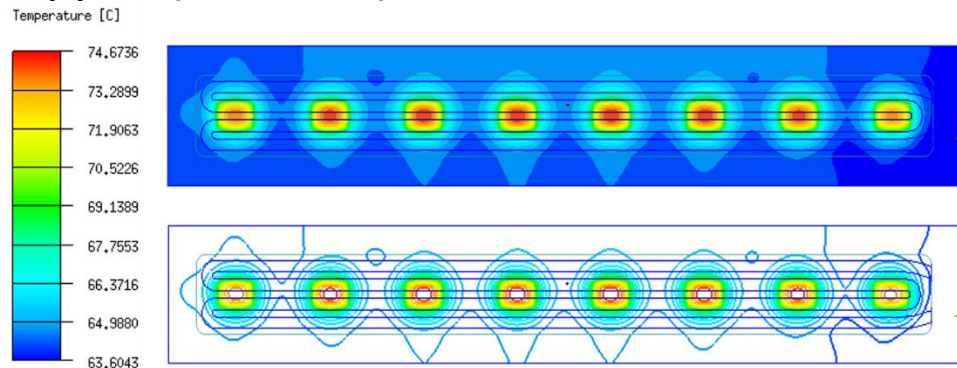
### Simulation results:

- Temperature contour plot and iso-thermal indicates low temperature gradient among the heat sources
- Sources 2 – 6 are at the same max. temperature (within 1 k deviation)
- Source 1 and source 8 max temperatures are slightly below
- The max temperatures show a temperature rise above ambient of less than 25 K

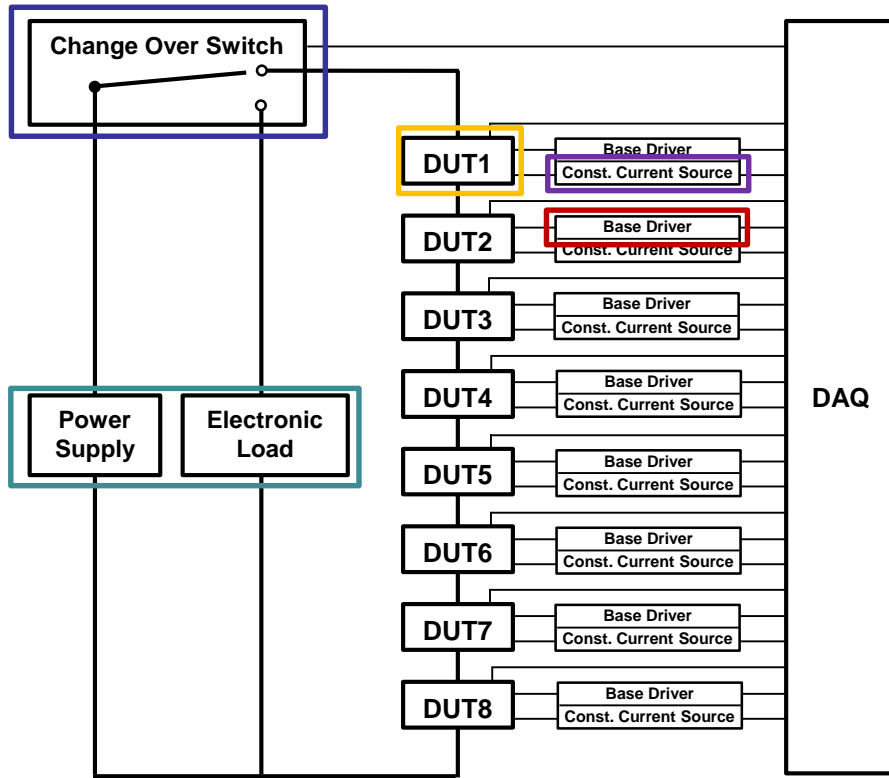
### Mid plane contour plots (top view):



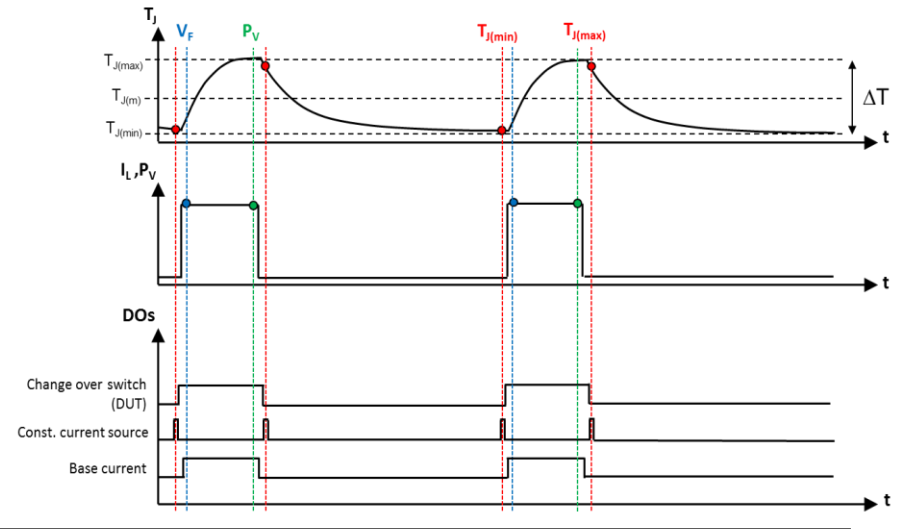
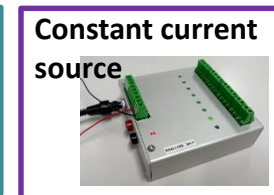
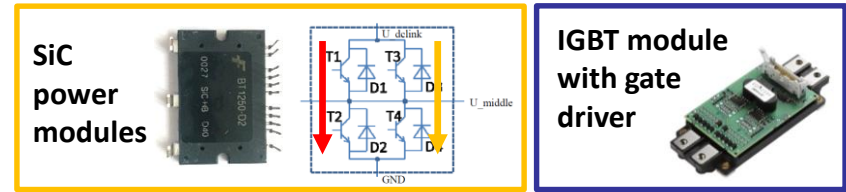
### Top plane (heat sources) contour:



# III. Reliability | Active power cycling: Connection plan



Test 1 Test 2



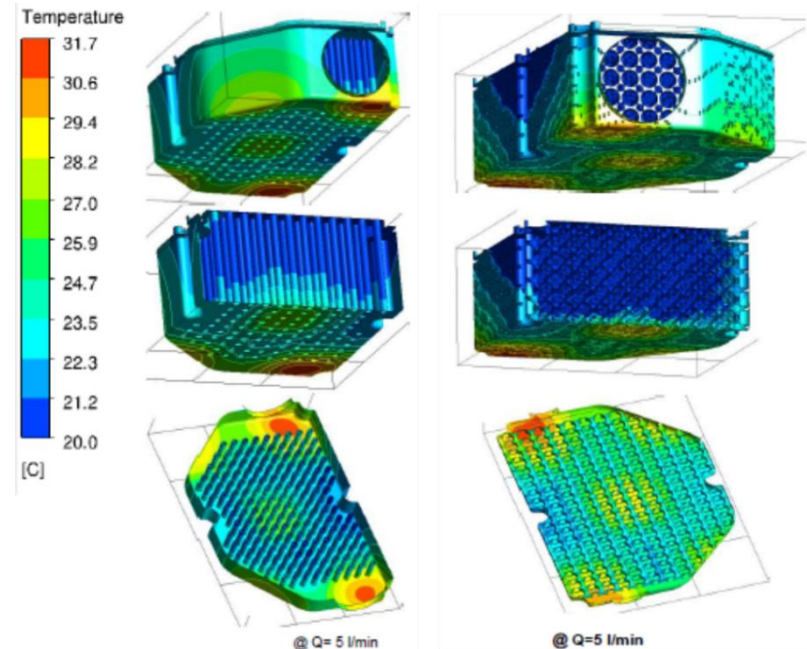
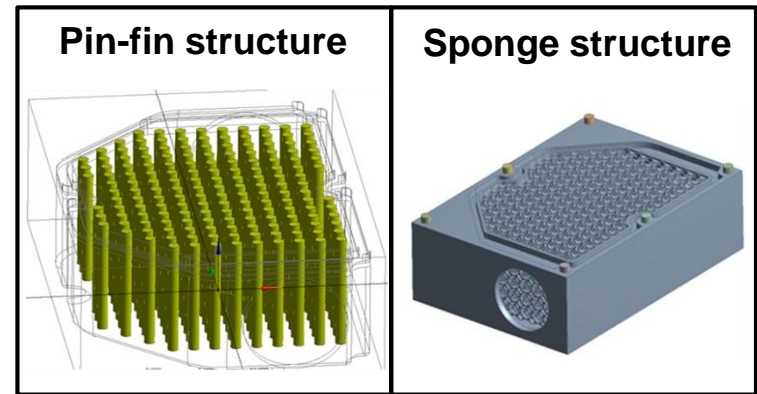


## IV. Novel cooling concepts

### Investigation of double-sided cooling concept (<sup>2</sup>COOL) by Swerea IVF:

- Thermal computational fluid dynamics (CFD) analyses on simple inline pin-fin structure as well as on sponge-like structure
  - Coolant flow: 5 – 15 l/min; Temp.: 20°C
  - Heat source: Single-sided scenario, 30W each
  - Results: see picture on the right; higher pressure drop for sponge-like structure

**Conclusion:** Further improvements needed in terms of reduced height and tilted sponge structure for better vertical mixing of coolant



## V. Next steps in COSIVU (reliability work for SiC power module)

### FE simulation:

- Simulation of active power cycles for single-sided power module
- Likewise, FE simulation for double-sided cooled power module
- Simulation at system level (inverter building block) with detailed sub-models of critical components (power module, current sensor, ...)

### Active power Cycling:

- Test bench adaptation:
  - Sample holder: Thermal fluid analysis on double-sided cooling system
  - Connection plan / HW: i) Finalization ii) Fully galvanic decoupled constant current sources iii) Base driver
  - Adaption of LabVIEW control software
- Power cycling tests and failure analysis on single-sided and double-sided cooled power modules

**Thank You for Your attention!**